



## Derivation of an energetically consistent Eddy-Diffusivity Mass-Flux scheme for oceanic convection

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## Context : "consistent" approach to the parameterization problem

[Gross et al. 2018, Eden & Iske 2019, Lauritzen et al. 2022]

Explicit assumptions + scale-separation operator

- achieve resolution-aware parameterizations
- consistent Energy Budgets



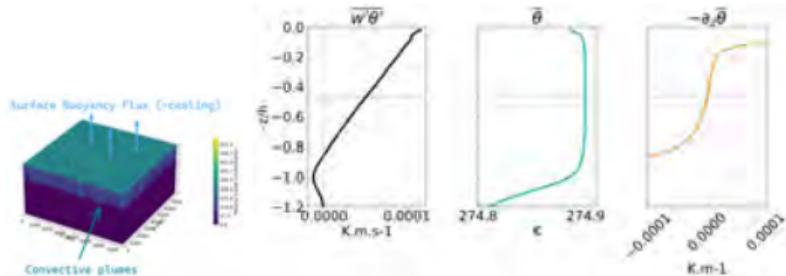
**Case study :** parameterization of the vertical flux  $\overline{w'\varphi'}$  in the boundary layer under the combined effect of local turbulence and convective plumes

# Inaccuracy of the eddy-diffusion approach ( $\overline{w'\theta'}^{\text{param}} = -K_\theta \partial_z \bar{\theta}$ )

For convection:

$$\overline{w'\theta'}^{\text{param}} = -K_\theta \partial_z \bar{\theta}$$

- ⇒ Transport by dense plumes not directly related to the local gradients
- ⇒ Need of '**non-local**' behavior [Deardorff 1966]



## Alternatives beyond eddy-diffusivity

- Use a "**gradient correction factor**" (a.k.a. *countergradient* term) :  $\overline{w'\theta'}^{\text{param}} = -K_\theta (\partial_z \bar{\theta} - \gamma_\theta)$
- **Non-Penetrative Convective adjustment schemes** [Killworth, 1989; Madec et al., 1991]
- **Coherent structures modeling** : Mass-flux schemes & Multi-fluid modeling
  - Atmosphere : [Hourdin et al., 2002; Siebesma et al., 2007; Tan et al., 2018; Thuburn et al., 2018 ...]
  - Ocean : proof of concept [Giordani et al., 2021]

Combined Eddy-Diffusivity Mass-Flux Approach:

- **Eddy-diffusivity (ED)**: small scale isotropic turbulence
- **Mass-flux (MF)**: direct contribution of coherent structures (= convective plumes) to fluxes

### Outline :

1. From Two-Fluid modeling to Mass-Flux Schemes
2. Horizontally averaged energy budgets (ED & MF coupling)
3. Practical implementation
4. Numerical experiments

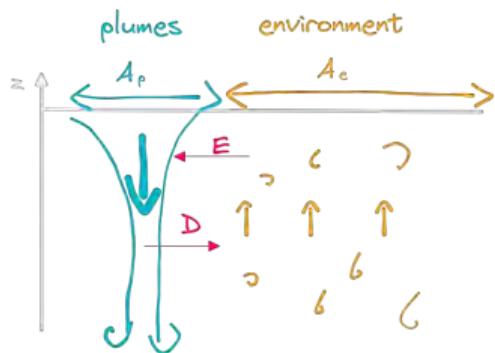
# 1

**Derivation of EDMF schemes starting from first principles**

## Two-domain decomposition

Decompose horizontal cell average into **plume** and **environment** averages

$$\bar{\phi} = a_p \phi_p + a_e \phi_e$$



$a_p, a_e$ : fractional areas of subdomains

$w_p, w_e$ : vertical velocities

$\phi_p, \phi_e$ : advected fields ( $u, v, \theta, S$ )

$E, D$ : horizontal entrainment/detrainment

## Decomposition of fluxes and plume averaged equations

① Apply this multi-fluid averaging to fluxes  $\overline{w' \phi'}$

$$\overline{w' \phi'} = \underbrace{a_p (w_p - \bar{w})(\phi_p - \bar{\phi})}_{\text{coherent structures}} + \underbrace{a_p \overline{w'_p \phi'_p}^p}_{\text{subdomain turbulence}} + \underbrace{a_e (w_e - \bar{w})(\phi_e - \bar{\phi})}_{\text{coherent structures}} + \underbrace{a_e \overline{w'_e \phi'_e}^e}_{\text{subdomain turbulence}}$$

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② Assume Eddy-Diffusivity in isotropic environment:

$$\overline{w' \phi'} \stackrel{\text{param}}{=} \underbrace{-K_\phi \partial_z \bar{\phi}}_{\text{subdomain turbulence}} + \underbrace{\frac{a_p}{1-a_p} w_p (\phi_p - \bar{\phi})}_{\text{coherent structures}}$$

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③ Subgrid plume model (steady plume hypothesis):

$$\frac{D}{Dt} \phi = \text{sources} \xrightarrow[\text{stationarity}]{(\cdot)^p} \partial_z (a_p w_p \phi_p) = E\phi_e - D\phi_p + a_p \text{ sources}$$

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④ Small area limit (?):

$$\partial_z (a_p w_p \phi_p) = E\bar{\phi} - D\phi_p + a_p \text{ sources},$$

$$\overline{w' \phi'} \stackrel{\text{param}}{=} K_\phi \partial_z \bar{\phi} + a_p w_p (\phi_p - \bar{\phi})$$

## Plume averaged equations

$\tilde{\alpha}$	$= \frac{1}{1 - a_p}$	Rescaling coefficient
$\frac{w' \phi'}{w' \mathbf{u}'_h}$	$= \tilde{\alpha} a_p w_p (\phi_p - \bar{\phi}) - K_\phi \partial_z \bar{\phi}$	Vertical turbulent flux for component $\phi$
	$= \tilde{\alpha} a_p w_p (\mathbf{u}_{h,p} - \bar{\mathbf{u}}_h) - K_m \partial_z \bar{\mathbf{u}}_h$	Vertical turbulent momentum flux
$\partial_z (a_p w_p)$	$= E - D$	Plume area conservation equation
$a_p w_p \partial_z \phi_p$	$= \tilde{\alpha} E (\bar{\phi} - \phi_p)$	Plume equation for component $\phi$
$a_p w_p \partial_z \mathbf{u}_{h,p}$	$= \tilde{\alpha} E (\bar{\mathbf{u}}_h - \mathbf{u}_{h,p}) + a_p w_p C_u \partial_z \bar{\mathbf{u}}_h$	Plume horizontal momentum equation
$a_p w_p \partial_z w_p$	$= -(\tilde{\alpha} b) E w_p + a_p \{ a B_p + \tilde{\alpha} (b'/h) w_p^2 \}$	Plume vertical velocity equation
$B_p$	$= b_{\text{eos}}(\phi_p) - b_{\text{eos}}(\bar{\phi})$	Buoyancy forcing term

- $\tilde{\alpha} = 1 \Leftrightarrow$  small area limit  $\rightarrow$  standard mass flux scheme

## Eddy-Diffusivity and Turbulent Kinetic Energy

'local' ED closure:  $\overline{w'\phi'} = -K_\phi \partial_z \bar{\phi}$

$K_\phi \propto l\sqrt{k}$  (one-equation turbulence models)

$K_\phi \propto k^2/\epsilon$  (second-order turbulence models)

with Turbulent Kinetic Energy (TKE):  $k = \frac{1}{2} \overline{\mathbf{u}' \cdot \mathbf{u}'}$

MF terms lead to energy exchanges

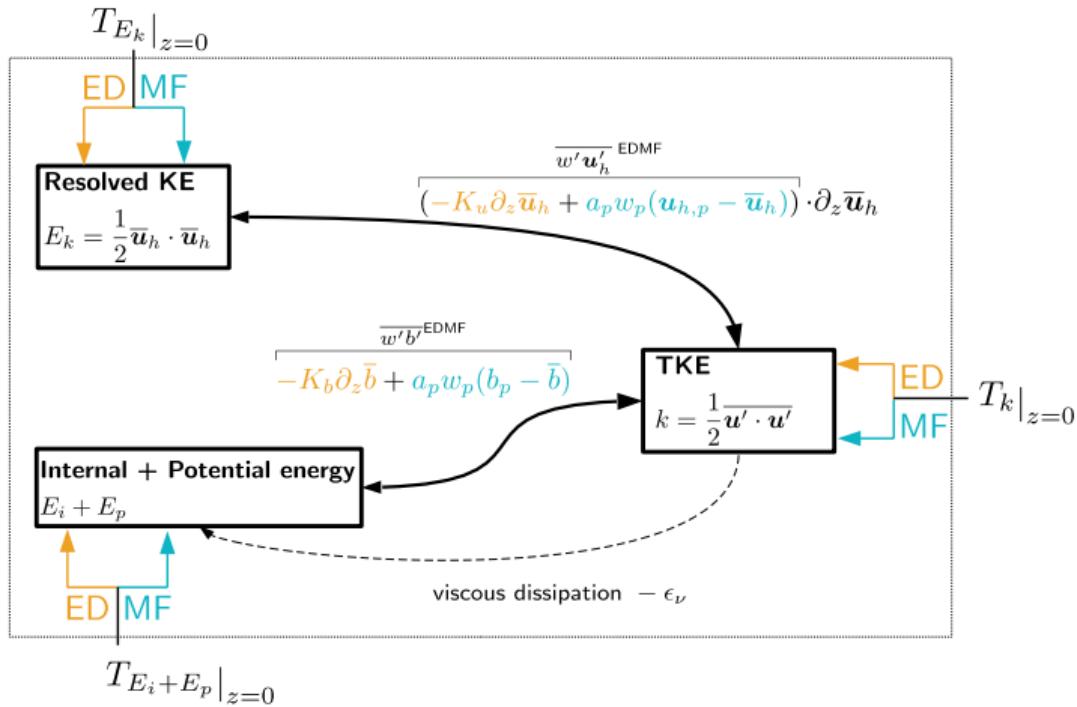
→ ED and MF are **not independent!**

Energy budgets enable coherent coupling

# 2

## Horizontally Averaged Energy budgets

# Bulk and boundary energy fluxes within EDMF closure



## Consistent energy budgets

Novelty for ocean (and atmosphere) EDMF: consistent TKE equation

$$\begin{aligned}\partial_t k - \partial_z (K_k \partial_z k) &= K_u (\partial_z \bar{\mathbf{u}}_h)^2 - K_\phi \partial_z \bar{b} && \text{ED related TKE production terms} \\ &\quad - a_p w_p (\mathbf{u}_{h,p} - \bar{\mathbf{u}}_h) \cdot \partial_z \bar{\mathbf{u}}_h + a_p w_p (b_p - \bar{b}) && \text{MF related TKE production terms} \\ &\quad - \partial_z \left( a_p w_p \left[ k_p - k + \frac{1}{2} \|\mathbf{u}_p - \mathbf{u}\|^2 \right] \right) && \text{MF related TKE transport term} \\ &\quad - \bar{\epsilon}_\nu && \text{TKE dissipation} \\ a_p w_p \partial_z k_p &= E \left( k - k_p + \frac{1}{2} \|\mathbf{u}_p - \mathbf{u}\|^2 \right) - a_p (\epsilon_\nu)_p && \text{Plume related TKE} \\ K_k &= c_k l_m \sqrt{k} && \text{TKE eddy-diffusivity}\end{aligned}$$

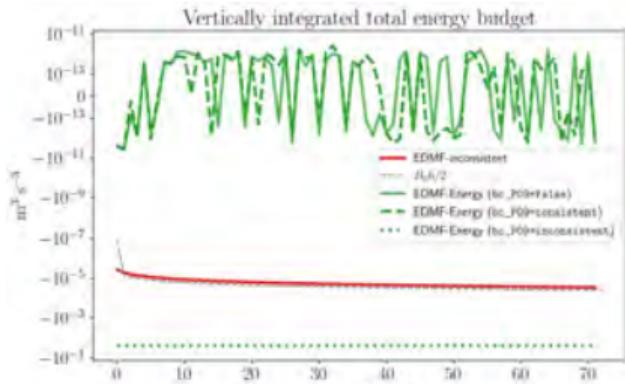
- Goes beyond existing literature (Witek et al., 2011a-b; Han & Bretherton, 2019) not motivated by considerations of energetic consistency

# Consistent energy budgets

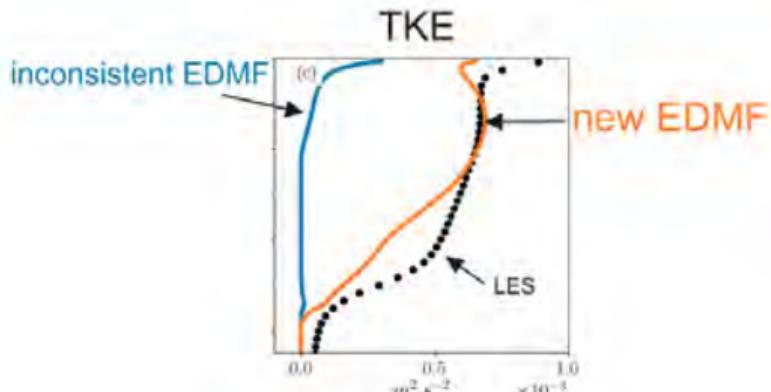
$$\begin{aligned}\partial_t k - \partial_z (K_k \partial_z k) &= K_u (\partial_z \bar{\mathbf{u}}_h)^2 - K_\phi \partial_z \bar{b} \\ &\quad - a_p w_p (\mathbf{u}_{h,p} - \bar{\mathbf{u}}_h) \cdot \partial_z \bar{\mathbf{u}}_h + a_p w_p (b_p - \bar{b}) \\ &\quad - \partial_z \left( a_p w_p \left[ k_p - k + \frac{1}{2} \|\mathbf{u}_p - \mathbf{u}\|^2 \right] \right) \\ &\quad - \bar{\epsilon}_\nu\end{aligned}$$

ED related TKE production terms  
MF related TKE production terms  
MF related TKE transport term  
TKE dissipation

→ Energy conservation



→ Significantly reduced TKE bias vs LES



# 3

## Practical implementation

## Discretization aspects

- Extension of the **energy-conserving discretization** by Burchard (2002) to the EDMF context
- Adapted for handling any unstable part of the density profile

"boundary layer-then-convection strategy"

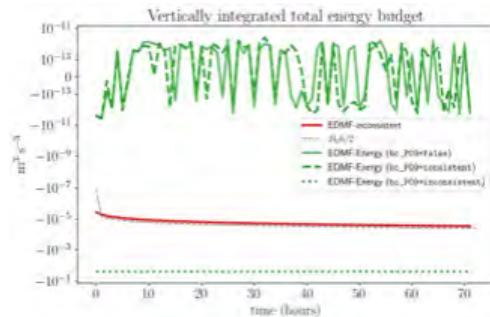


Figure: Time series of the vertically integrated energy budget for the case W005\_C500.

ED step

$$\begin{aligned}\phi^{n+1,*} &= \phi^n + \Delta t \partial_z (K_\phi(k^n, b^n) \partial_z \phi^{n+1,*}) \\ \mathbf{u}_h^{n+1,*} &= \mathbf{u}_h^n + \Delta t \partial_z (K_{\mathbf{u}}(k^n, b^n) \partial_z \mathbf{u}_h^{n+1,*}) \\ b^{n+1,*} &= b_{\text{eos}}(\phi^{n+1,*})\end{aligned}$$

MF step

$$\begin{aligned}[a_p, w_p, \phi_p, \mathbf{u}_{h,p}, k_p, B_p] &= \text{MF}(b^{n+1,*}, \mathbf{u}_h^{n+1,*}) \\ \phi^{n+1} &= \phi^{n+1,*} - \Delta t \partial_z (a_p w_p (\phi_p - \phi^{n+1,*})) \\ \mathbf{u}_h^{n+1} &= \mathbf{u}_h^{n+1,*} - \Delta t \partial_z (a_p w_p (\mathbf{u}_{h,p} - \mathbf{u}_h^{n+1,*}))\end{aligned}$$

TKE update

$$k^{n+1} = k^n + \Delta t \partial_z (K_k \partial_z k^{n+1}) + \mathcal{F}_k(b^{n+1}, \mathbf{u}_h^{n+1}, \mathbf{u}_h^n, \dots)$$

# 4

## Numerical experiments

# A collection of LES cases

In collaboration with B. Deremble, IGE, Grenoble (TRACCS project)

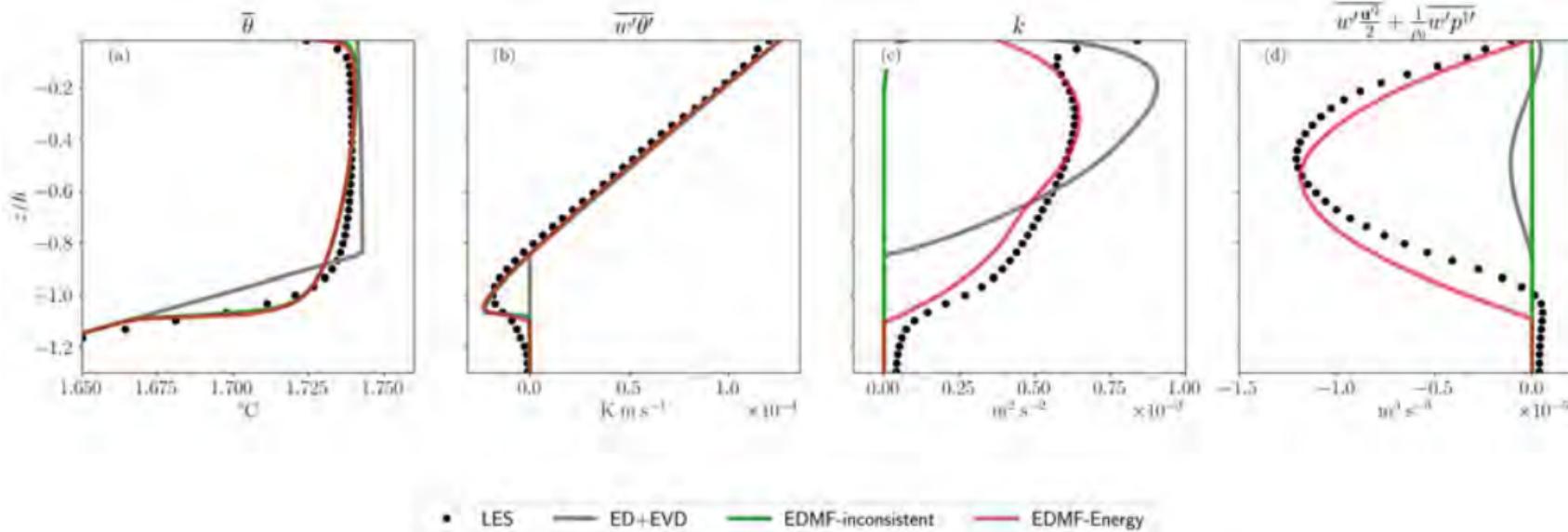
Case	heat flux W m <sup>-2</sup>	swrad W m <sup>-2</sup>	wind Pa	E-P mm day <sup>-1</sup>	Coriolis s <sup>-1</sup>	Ini. ML	Model
FC075	-75	0	0	0	0	no	NCAR-LES
FCML075	-75	0	0	0	0	yes	NCAR-LES
FC500	-500	0	0	0	0	no	Meso-NH/Croco
W05_C500	-500	0	0.5	0	0	no	Meso-NH
W005_C500	-500	0	0.05	0	0	no	Meso-NH/Croco
W01_EC75	-75	0	0.1	1.37	$10^{-4}$	no	NCAR-LES
DC	-75	235	0.	1.37	0	no	NCAR-LES
WANG1	-111	0	0	0	$1.26 \times 10^{-4}$	yes	Meso-NH
W05_C100	-100	0	0.5	0	$1.06 \times 10^{-4}$	no	Meso-NH/Basilisk
W05_C200	-200	0	0.5	0	$1.06 \times 10^{-4}$	no	Meso-NH/Basilisk
W081_W150	150	0	0.81	0	$1.06 \times 10^{-4}$	no	Meso-NH/Basilisk

+ preliminary tests with **TLab** (J. P. Mellado et al.) and **Oceananigans**

+ Realistic case : Hymex/ASICS-MED campaign (Giordani et al., 2021)

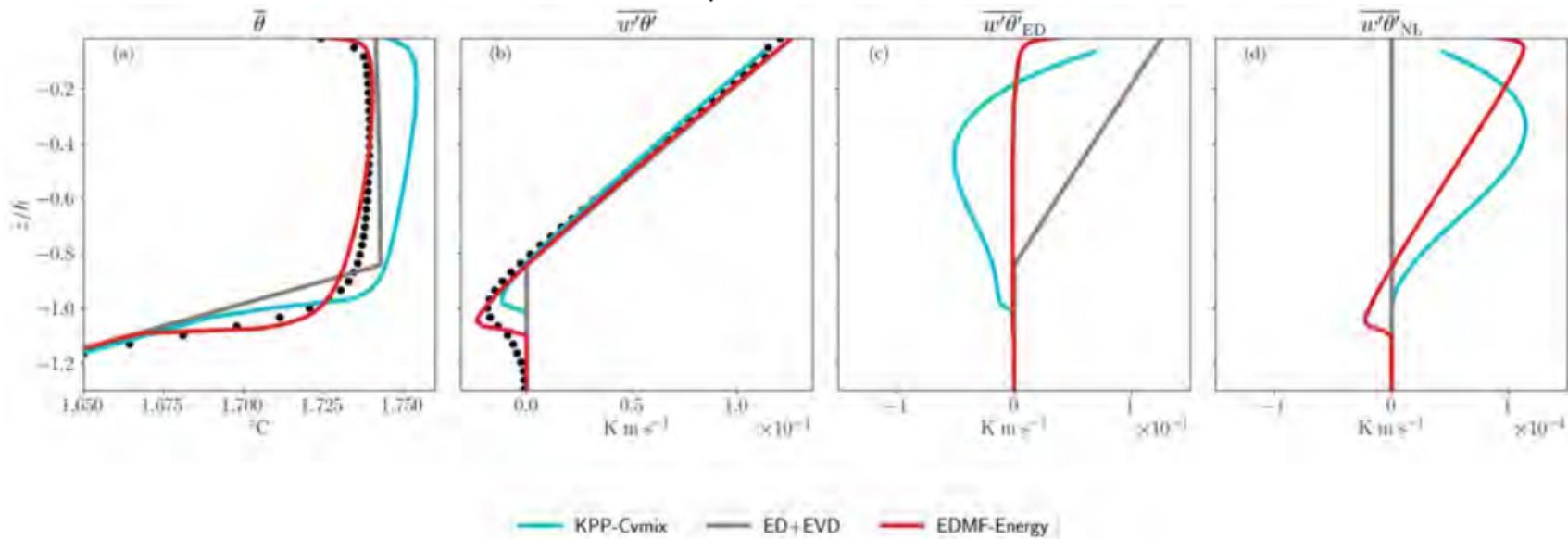
## Example 1 : FC500 case

Instantaneous profiles after 72 hours

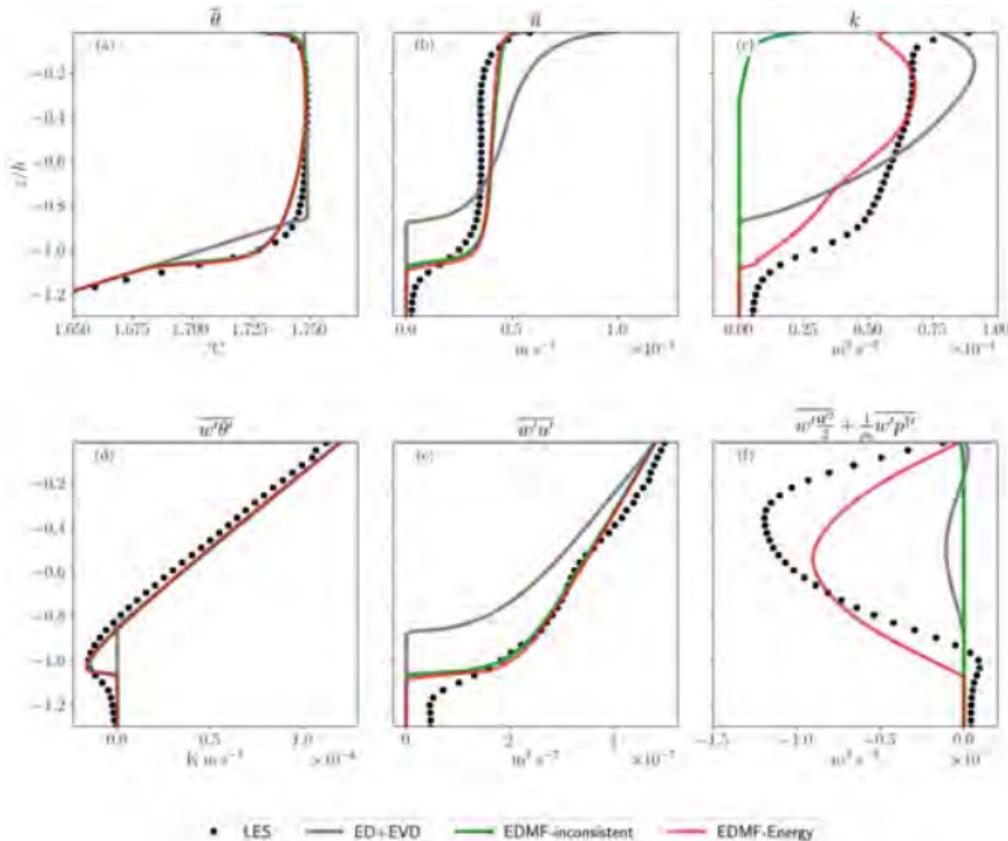


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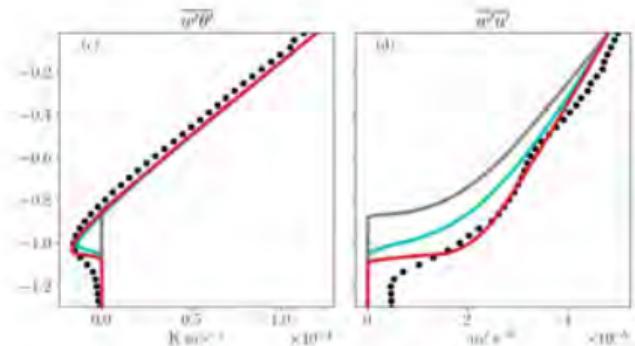
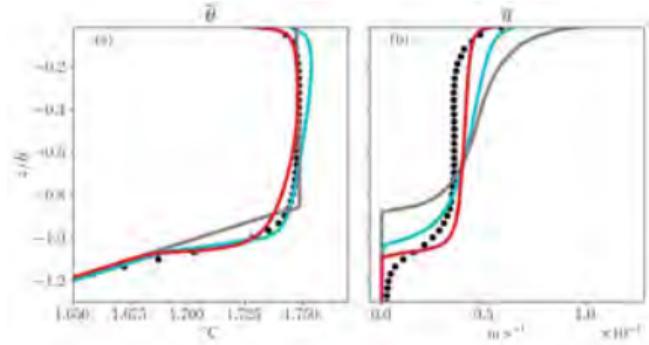
Instantaneous profiles after 72 hours



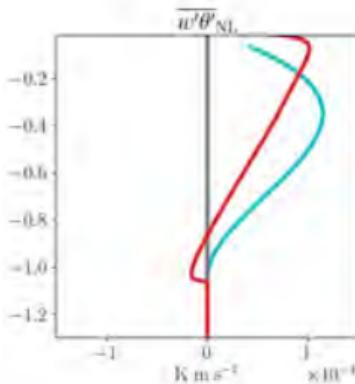
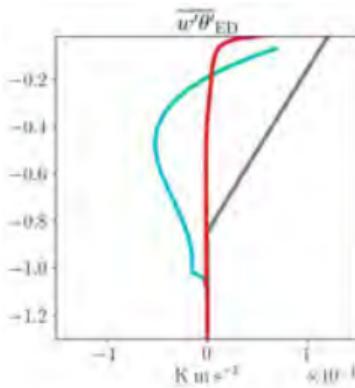
## Example 2 : W005\_C500 case (Instantaneous profiles after 72 hours)



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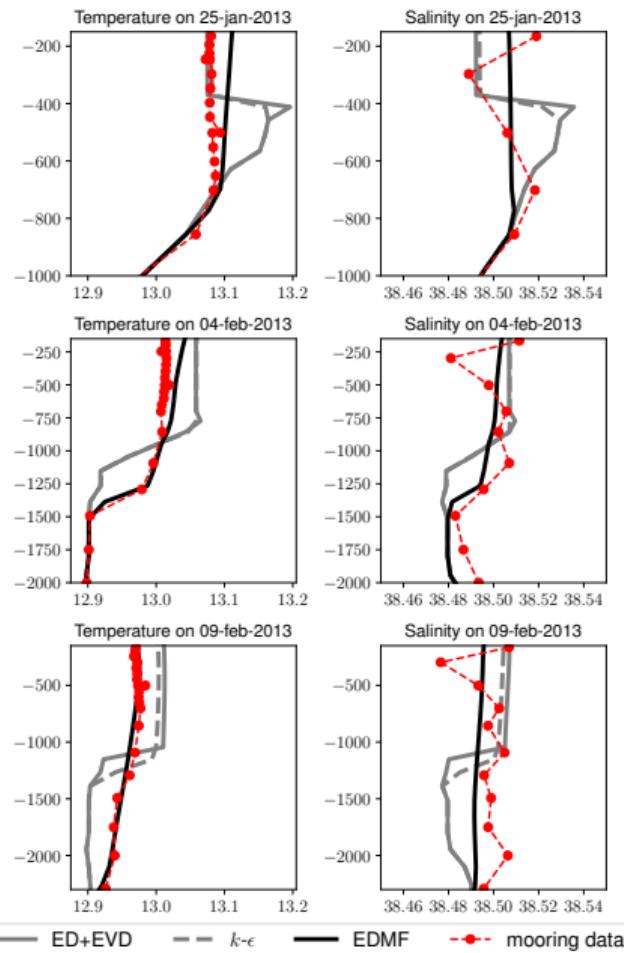
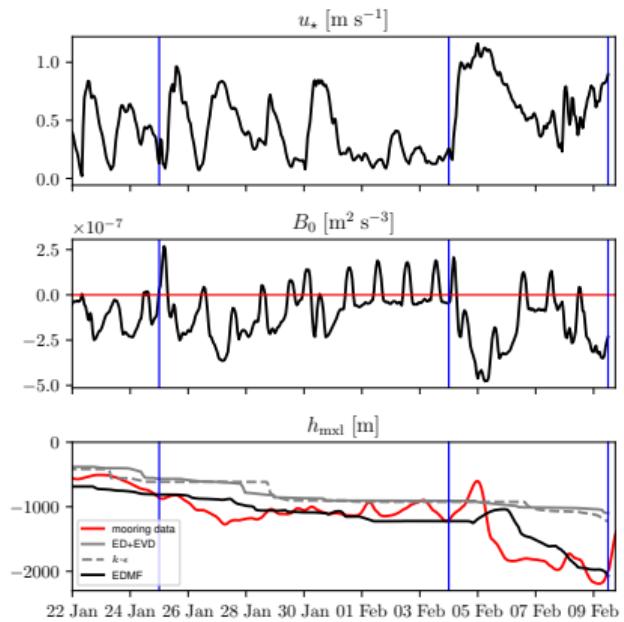


• LES    — KPP-Cvmax    — ED+EVG    — EDMF-Energy



# HyMeX/ASICS-MED experiment (LION buoy)

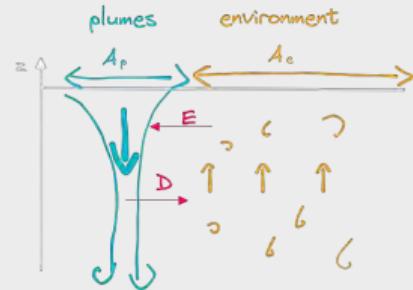
Sequence of strong convective events in the Northwestern Mediterranean during the winter 2013.



# Summary

## Eddy-Diffusivity Mass-Flux (EDMF) parameterization for convection

$$\overline{w'\phi'}^{\text{param}} = \underbrace{-K_\phi \partial_z \bar{\phi}}_{\text{local turbulent mixing}} + \underbrace{a_p w_p (\phi_p - \bar{\phi})}_{\text{nonlocal transport by coherent structures}}$$



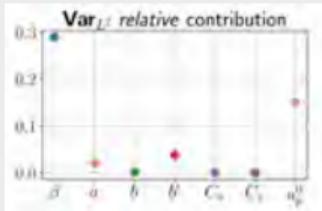
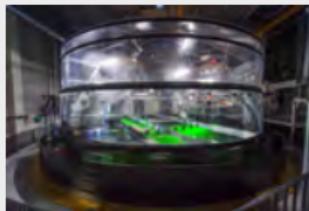
- ✓ PDE-based derivation and explicit assumptions
- ✓ Flexible multi-fluid averaging framework
- ✓ Fully-consistent Subgrid+Resolved energy budgets
- ✓ Evaluation in a SCM against LES simulations and observational data.

■ M. Perrot, F. Lemarié & T. Dubos. *Energetically consistent Eddy-Diffusivity Mass-Flux schemes. Part I: Theory and Models*, 2024. under review in JAMES

■ M. Perrot & F. Lemarié. *Energetically consistent Eddy-Diffusivity Mass-Flux schemes. Part II: implementation and evaluation in an oceanic context*, 2024. under review in JAMES

## In progress

- ▷ Sensitivity analysis
- ▷ Parameter estimation (w. O. Zahm et al.)
- ▷ Reference data : LES simulations & laboratory experiments (PLUME project)



- ▷ Implementation in **Croc** (Med. Sea operational configuration)
- ▷ Implementation in **MesoNH** (atmosphere)
- ▷ Coupling with parameterization of **restratification processes**

